An aerial photograph showing a flooded residential neighborhood. Houses and trees are partially submerged in dark water. In the upper right, a large blue steel truss bridge spans the water. The sky is overcast and grey.

# **Preliminary Analysis of Self-Cleaning Capacity of Lake Pontchartrain using Fugacity Analysis**

**MESL RESEARCH GROUP**

**S. Kilic, K. Nam and M. Aral**

# Hurricane Katrina



# A Devastated City



# Short Term Solutions to Drain The City of New Orleans



# Is Dilution Really the Solution?



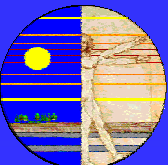
# How Long will it take Lake Pontchartrain to replenish itself?



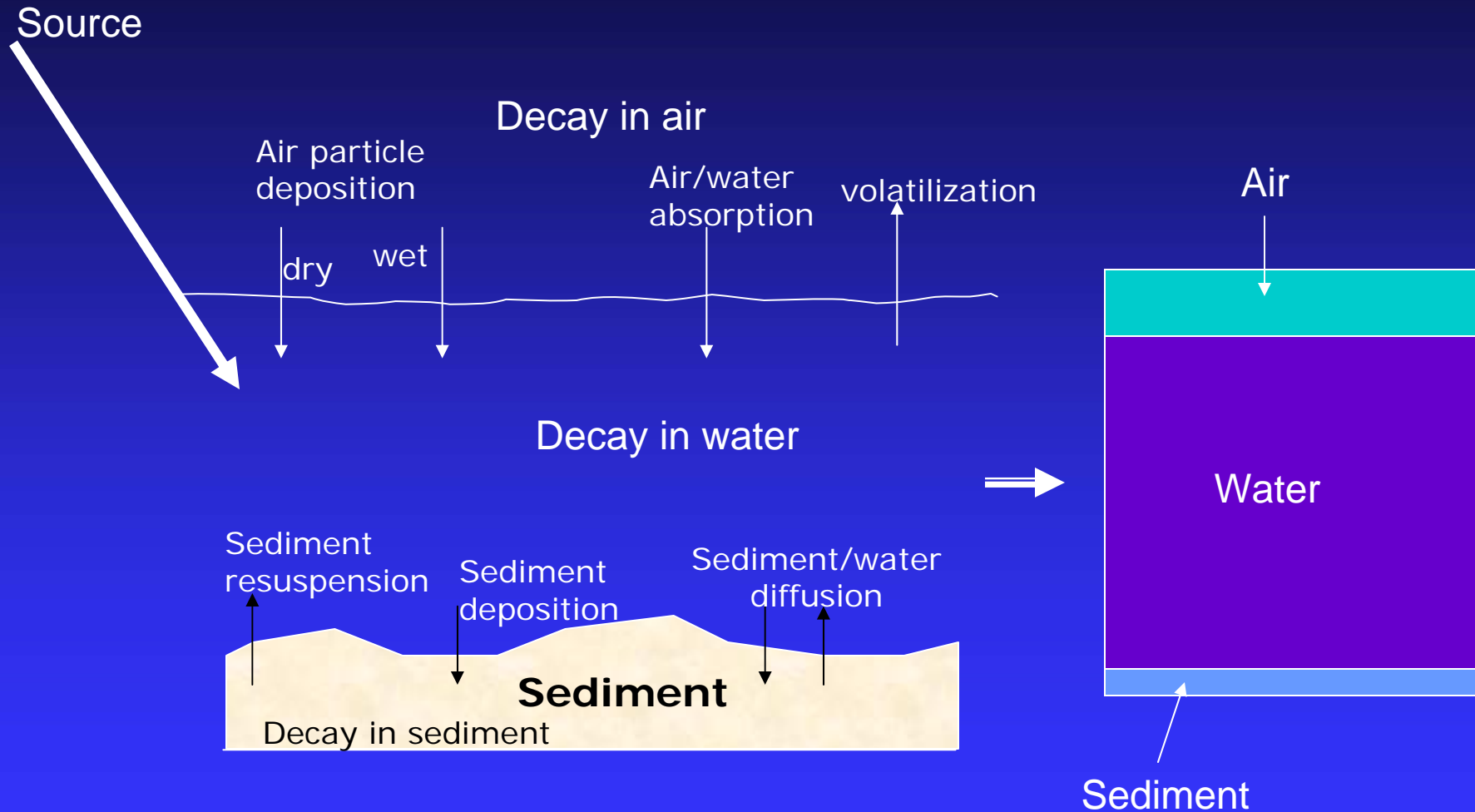


# Objective

- How long will it take Lake Pontchartrain to be “clean” again?
- The mechanisms involved
  - Dilution
  - Decay
  - Volatilization – removal by winds
  - Deposition
  - Removal with outflow



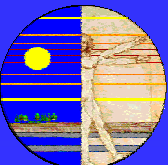
# Natural Processes in the Lake





# Natural Processes in the Lake

- In the water:
  - Source
  - Deposition from air
  - Resuspension from sediment
  - First order decay
  - Outflow from lake
- In the air:
  - Volatilization from water
  - First order decay
  - Wind induced air flow out of the lake system
- In the sediment:
  - Deposition from water
  - Diffusion between water
  - First order decay



# Mathematical Model

$$V_w Z_{bw} \frac{dF_w}{dt} = E_w + (K_{aw} A_w Z_w + Q_{dry} Z_{aerosol} + Q_{wet} Z_{aerosol}) F_A + (Q_{res} Z_s + K_{sw} A_s Z_w) F_S - (k_w V_w Z_w + Q_{dep} Z_p + Q_{out} Z_{bw} + K_{aw} A_w Z_w) F_W$$

Water  
Phase

$$V_a Z_{aw} \frac{dF_A}{dt} = (K_{aw} A_w Z_w) F_W - (Q_{dry} Z_{aerosol} + k_a V_a Z_a + Q_{wet} Z_{aerosol} + Q_{air} Z_{ba} + K_{aw} A_w Z_w) F_A$$

Air  
Phase

$$V_s Z_{bs} \frac{dF_S}{dt} = (Q_{dep} Z_p + K_{sw} A_s Z_w) F_W - (k_s V_s Z_s + Q_{res} Z_s + K_{sw} A_s Z_w) F_S$$

Sediment  
Phase



# Parameters Used in the Model

- $F_w$  : water fugacity
- $F_a$  : air fugacity
- $F_s$  : sediment fugacity
- $V_w$  : volume of water
- $V_a$  : volume of air
- $V_s$  : volume of sediment
- $A_w$  : water surface area
- $A_s$  : sediment surface area
- $Q_{out}$  : outgoing water flowrate
- $Q_{air}$  : air flowrate
- $Q_{dep}$  : particle deposition rate
- $Q_{res}$  : sediment resuspension rate
- $Q_{dry}$  : dry air deposition rate
- $Q_{wet}$  : wet air deposition rate
- $t$  : time
- $K_{aw}$  : water-air mass transfer coefficient
- $K_{sw}$  : sediment-water mass transfer coefficient
- $k_w$  : water decay constant
- $k_a$  : air decay constant
- $k_s$  : sediment decay constant
- $Z_w$  : water fugacity capacity
- $Z_a$  : air fugacity capacity
- $Z_s$  : sediment fugacity capacity
- $Z_p$  : water particle fugacity capacity
- $Z_{aerosol}$  : aerosol fugacity capacity
- $Z_{bw}$  : bulk water fugacity capacity
- $Z_{ba}$  : bulk air fugacity capacity
- $Z_{bs}$  : bulk sediment fugacity capacity



# Information Required to Solve the Governing Equations

- Information about the lake
  - Volume of lake, sediments, and air parcel
  - Surface area
  - Flow rate of outgoing tributaries
  - Air flow rate
  - Sediment deposition rate
  - Sediment resuspension rate
  - Dry deposition rate
  - Wet deposition rate
- Information about the content of the flood waters



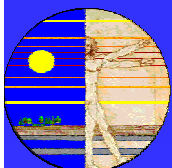
# The Contents of the Flood Waters

No information



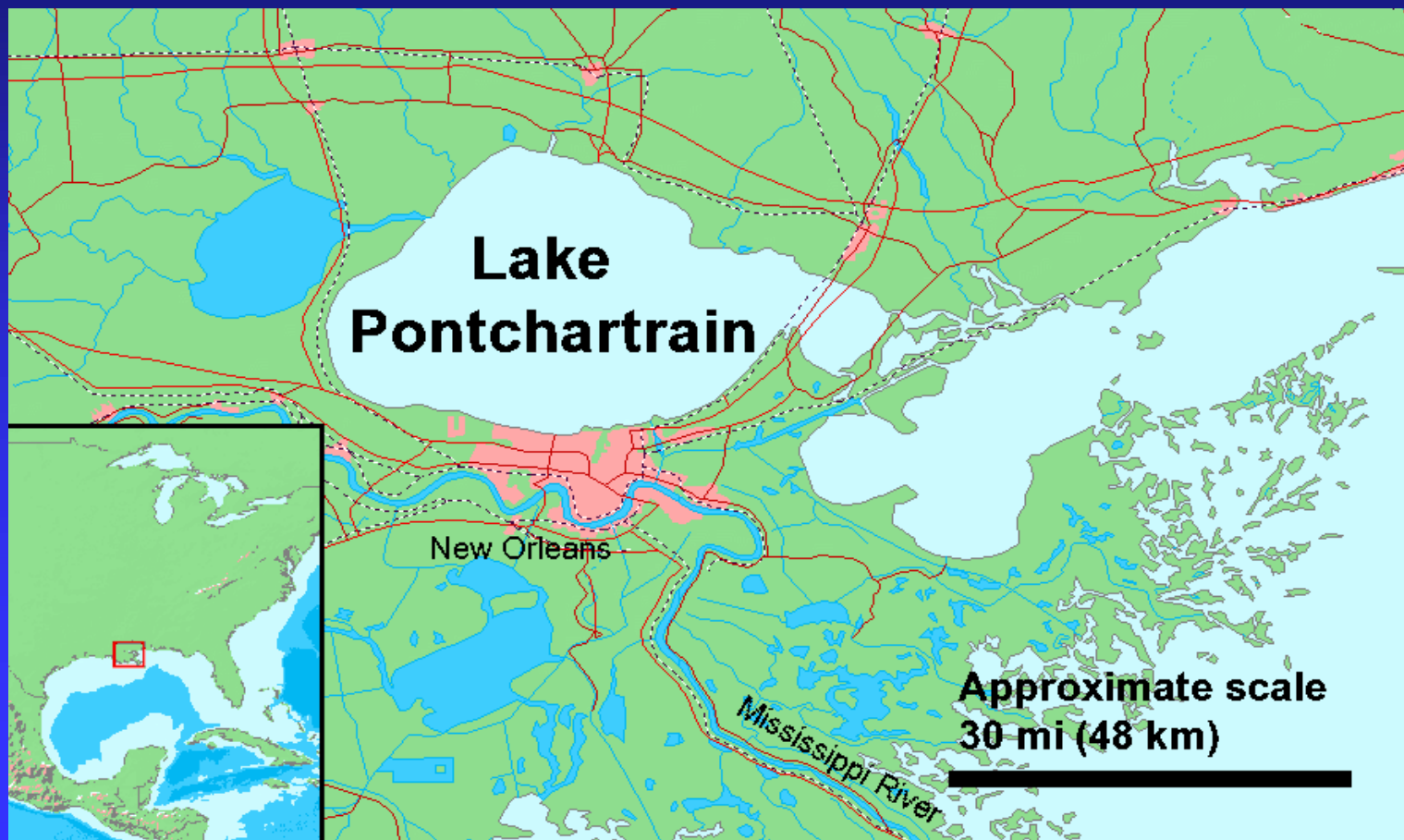
# Contaminants Selected for this Study

- **Benzene**
  - Volatile, primary pollutant, commonly used, health issues
- **Lindane**
  - Pesticide, used commonly by agricultural practice, health issues
- **PCBs**
  - Primary pollutant, recalcitrant, toxic, bioaccumulative



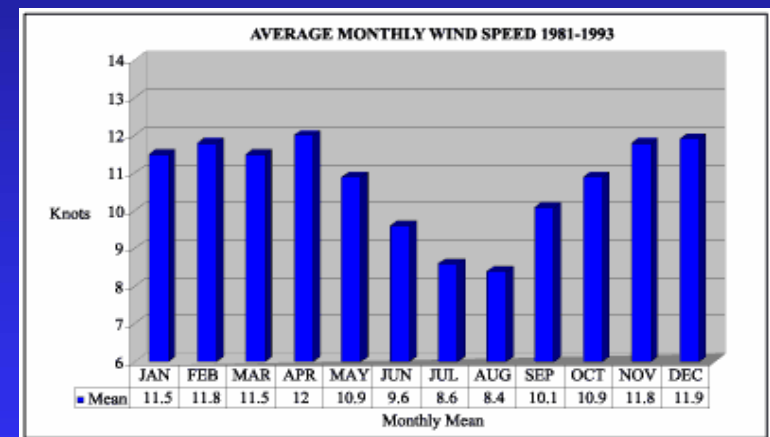
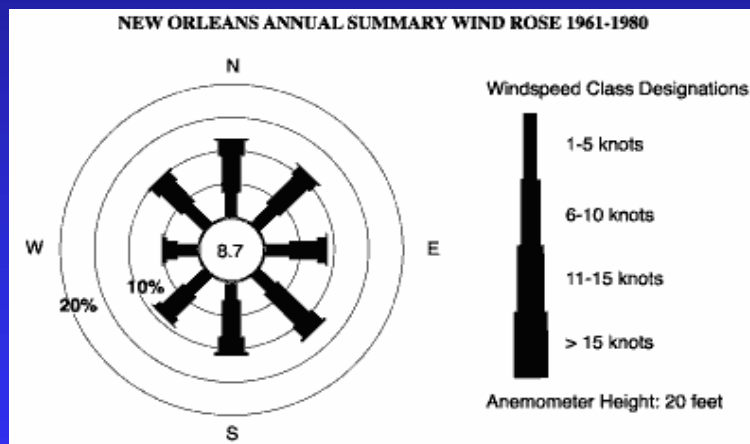
# Lake Pontchartrain

Surface Area	: 1632000000 m <sup>2</sup> (630 mi <sup>2</sup> )
Average Depth	: 3.65 m (12 ft)
Total water outflow	: 1563352 m <sup>3</sup> /h (15336 cfs)
Wind speed on lake	: 10.75 knots (19908.83 m/h)
Depth of air on lake	: 0.5 m
Volume of air	: 816000000 m <sup>3</sup>
Depth of sediment	: 0.05 m
Volume of sediment	: 81600000 m <sup>3</sup>
Density of sediment	: 2400 kg/m <sup>3</sup>

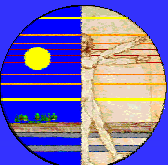




# Wind induced advection above Lake Pontchartrain



$$Q_{air} = 32000000 \text{ m}^3/\text{hour}$$



# Deposition and Resuspension Rates

- Adopted from a Steady-State Fugacity model development in Trent University:
  - $U_{\text{deposition}} = 0.0000005 \text{ m/h}$
  - $U_{\text{resuspension}} = 0.0000002 \text{ m/h}$
  - $Q_{\text{dry air deposition}} = 2.76 \text{ m/hour}$
  - $Q_{\text{wet air deposition}} = 7.34 \text{ m/hour}$

(<http://www.trentu.ca/cemc/models>)



# Mass Transfer Coefficients

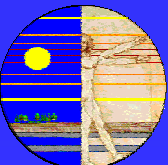
- Two-film theory to calculate for each contaminant
- Overall water-air mass transfer coefficient:

$$\frac{1}{K_{aw}} = \frac{1}{k_{water}} + \frac{1}{k_{air}H}$$

**$K_{aw} = 0.0034$  m/hour for PCBs**

**$K_{aw} = 0.00002$  m/hour for Lindane**

**$K_{aw} = 0.00958$  m/hour for Benzene**



# Physicochemical Properties Required for Contaminants

- Water Solubility
- Vapor Pressure
- Octanol-Water Partition Coefficient
- Density
- Molecular Weight
- Half lives in each media

$$Z_{air} = \frac{1}{RT}$$

$$Z_{water} = \frac{1}{H} = \frac{C^s}{P_s}$$

$$Z_{sediment} = \frac{K_{sw}\rho_s}{H} = K_{sw}\rho_s(Z_{water})$$

$$k_{reaction} = \frac{\ln 2}{\tau_{1/2}}$$



# Source Rate

- The pumping lasted about one week
- About 10% of lake volume was pumped into the lake
- 3420000 m<sup>3</sup>/hour source rate
- 10 % of the dumped water is contaminant by volume.
- Convert to mass rate for each contaminant
  - 22000000000 moles/hour Lindane
  - 38400000000 moles/hour Benzene
  - 14700000000 moles/hour PCB



# Solution Technique of the System of Equations

- The nonlinear model yields three equations with three unknowns.
- Finite Difference Method is used to solve the governing equations.
- A matrix solution algorithm is developed for simultaneous solution.



# Final Values Used in the Model

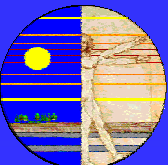
Deposition Rate	816 m <sup>3</sup> /h		
Resuspension Rate	326 m <sup>3</sup> /h		
Dry air deposition rate	2.76 m <sup>3</sup> /h		
Wet air deposition rate	7.34 m <sup>3</sup> /h		
	PCB	LINDANE	BENZENE
Air-water MTC (m/h)	0.0034	0.0002	0.00958
Sediment-water MTC (m/h)	0.0001	0.0004	0.0006
Water decay rate (1/h)	$5 \times 10^{-6}$	$4.08 \times 10^{-5}$	$4.08 \times 10^{-2}$
Air decay rate (1/h)	0.0001	$4.08 \times 10^{-3}$	$4.08 \times 10^{-3}$
Sediment decay rate (1/h)	$2 \times 10^{-6}$	$1.26 \times 10^{-5}$	$4.08 \times 10^{-4}$



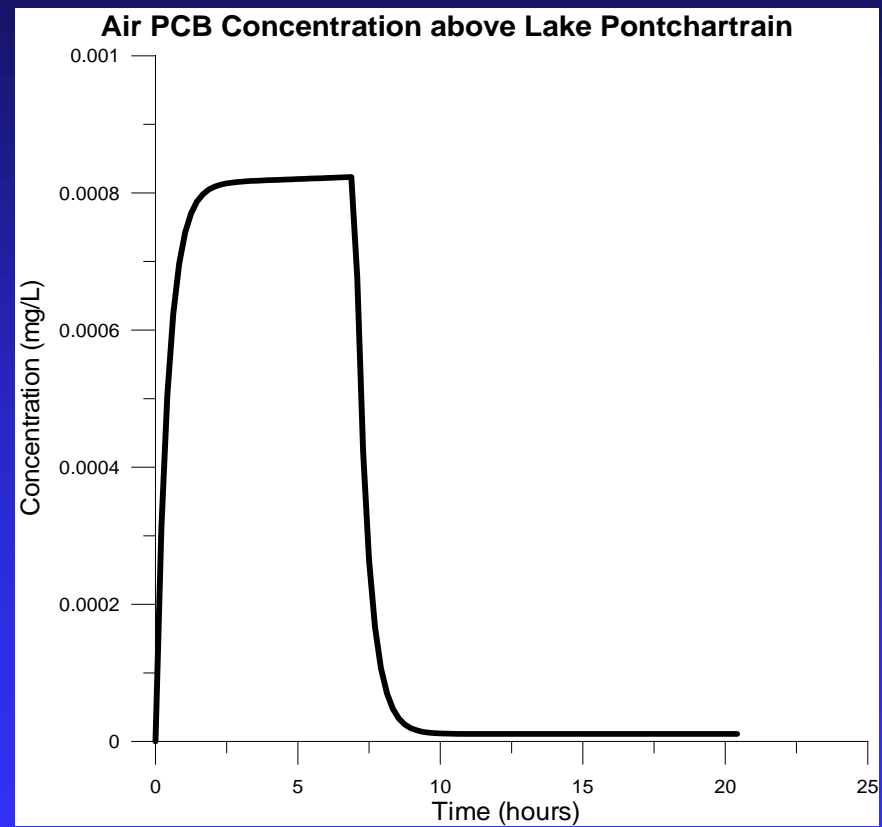
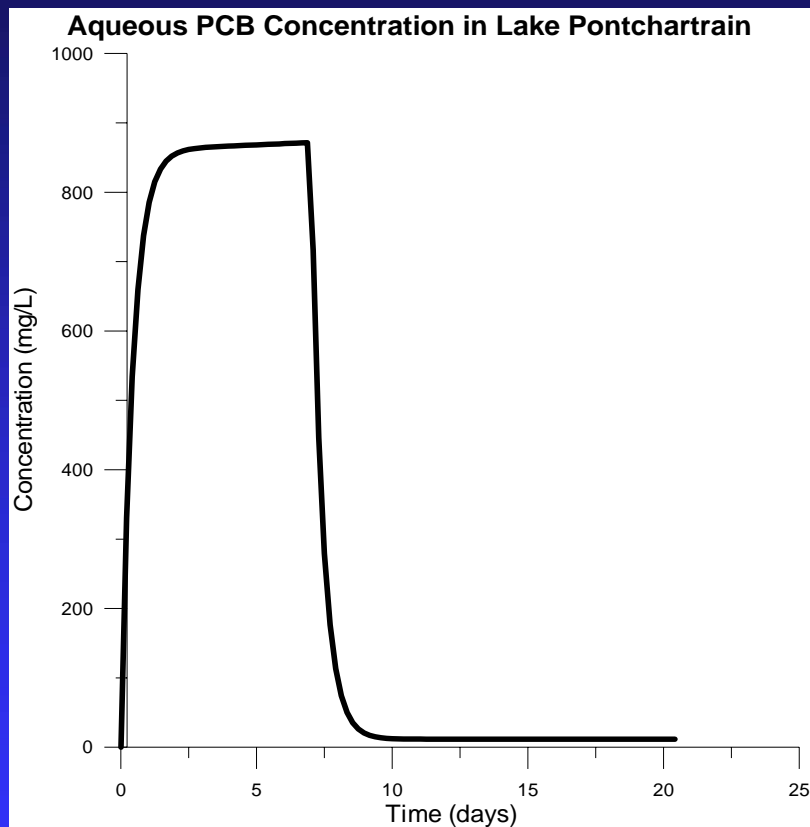


# Results

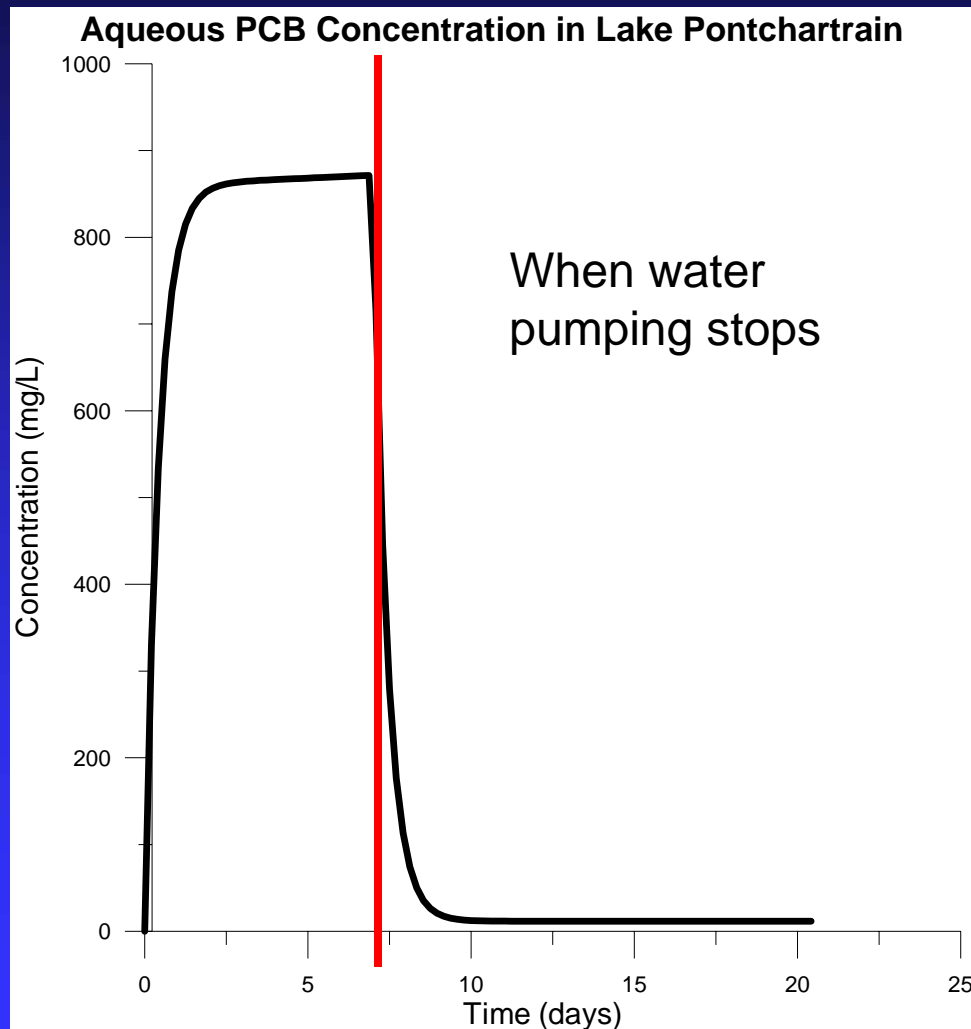
- It will take Lake Pontchartrain:
  - 1 year to recover from Benzene pollution.
  - 13.5 years to recover from Lindane pollution.
  - 81 years to recover from PCB pollution.
- Regulated standard values by EPA in water:
  - Benzene 0.005 mg/L.
  - Lindane 0.0002 mg/L.
  - Total PCBs 0.0005 mg/L.



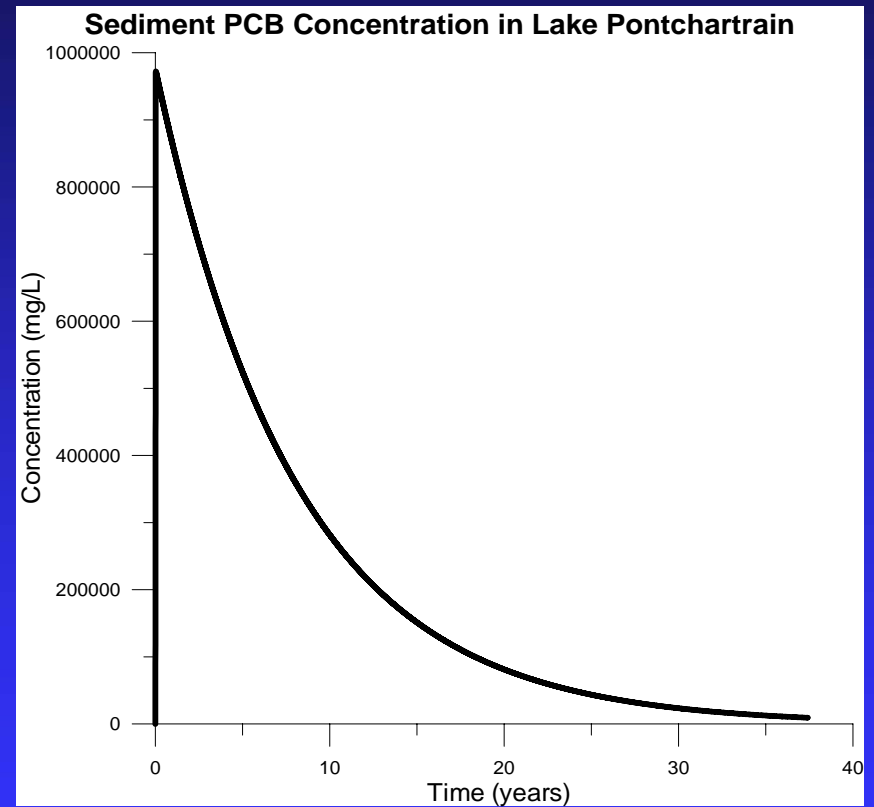
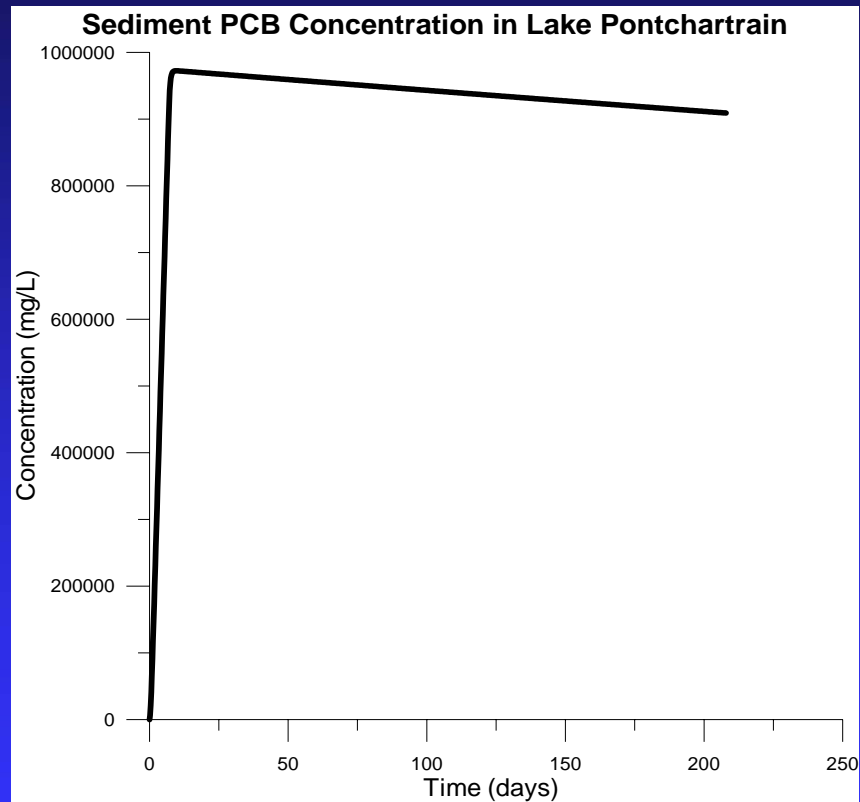
# PCB Results



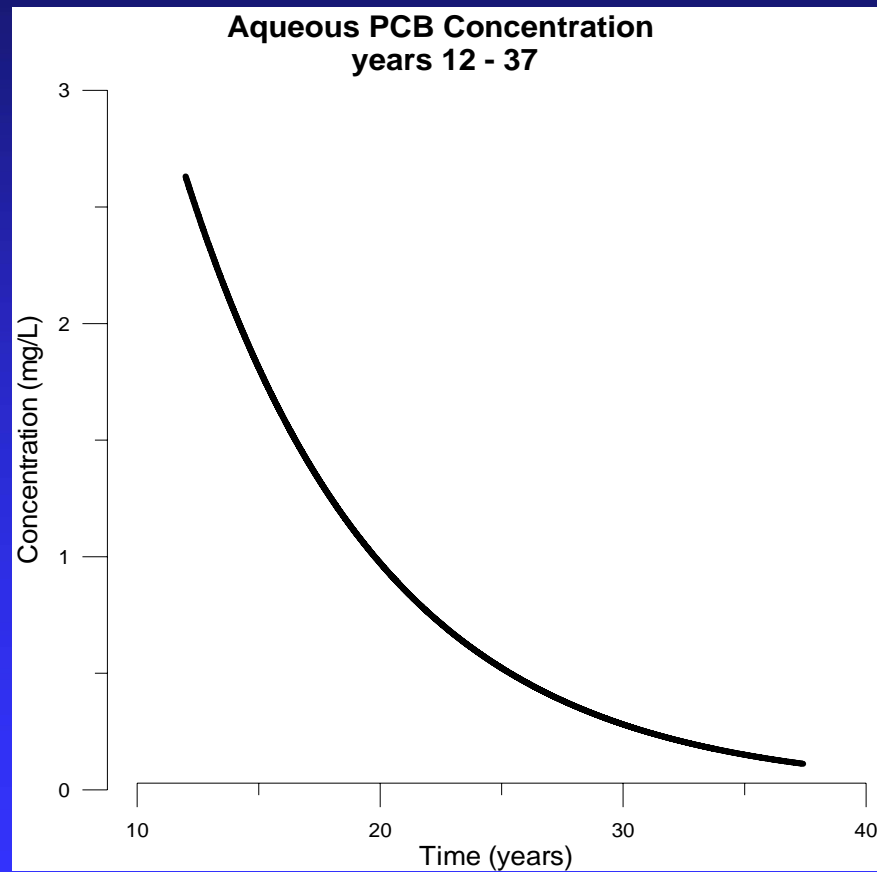
# How Lake Pontchartrain Reacts to Contaminant Dumping Water



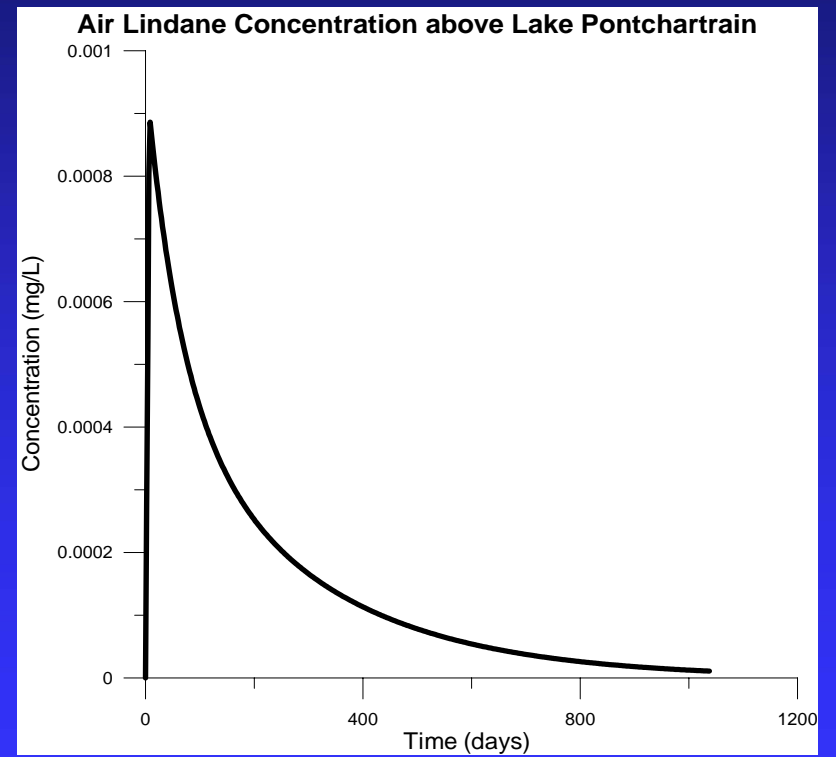
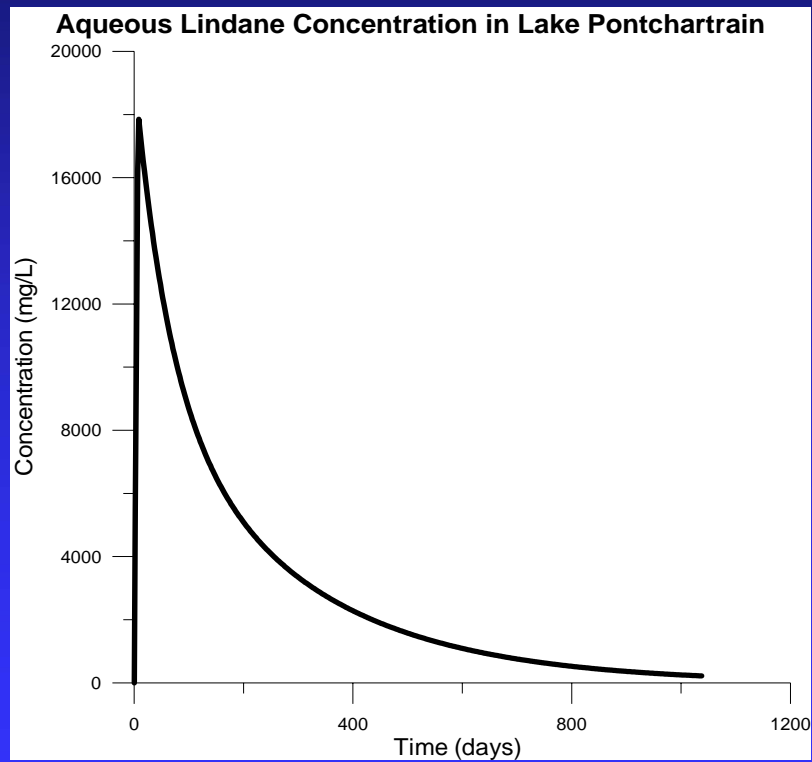
# PCB Results



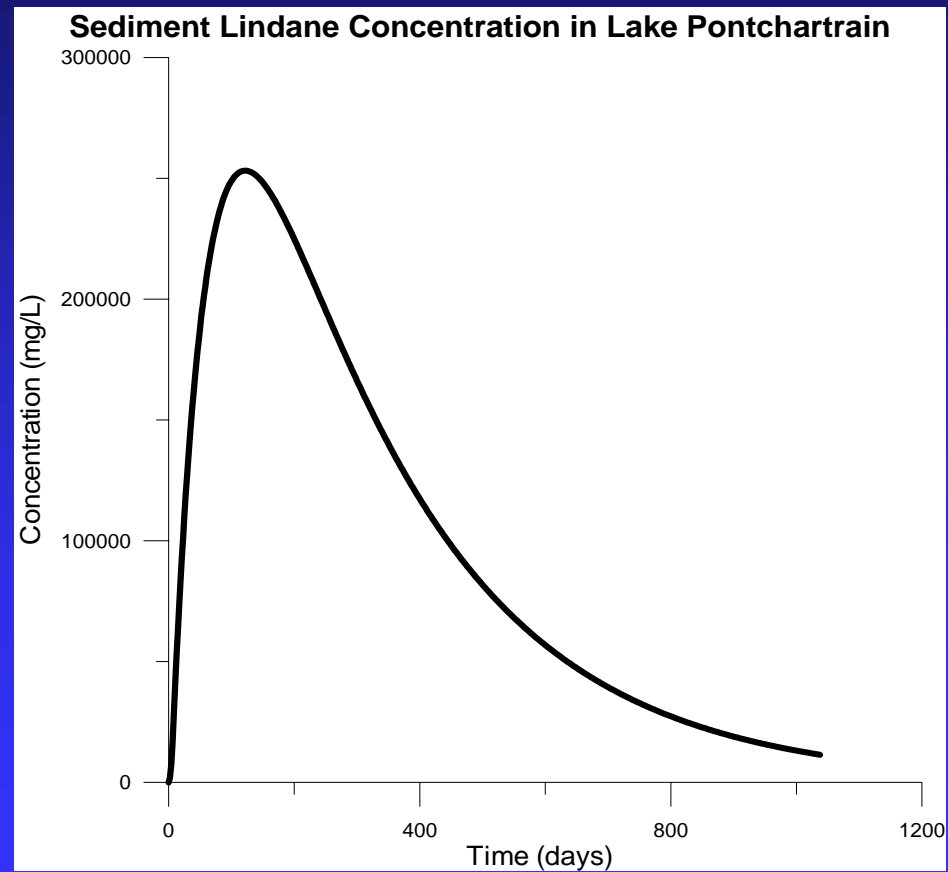
# PCB Results



# Lindane Results

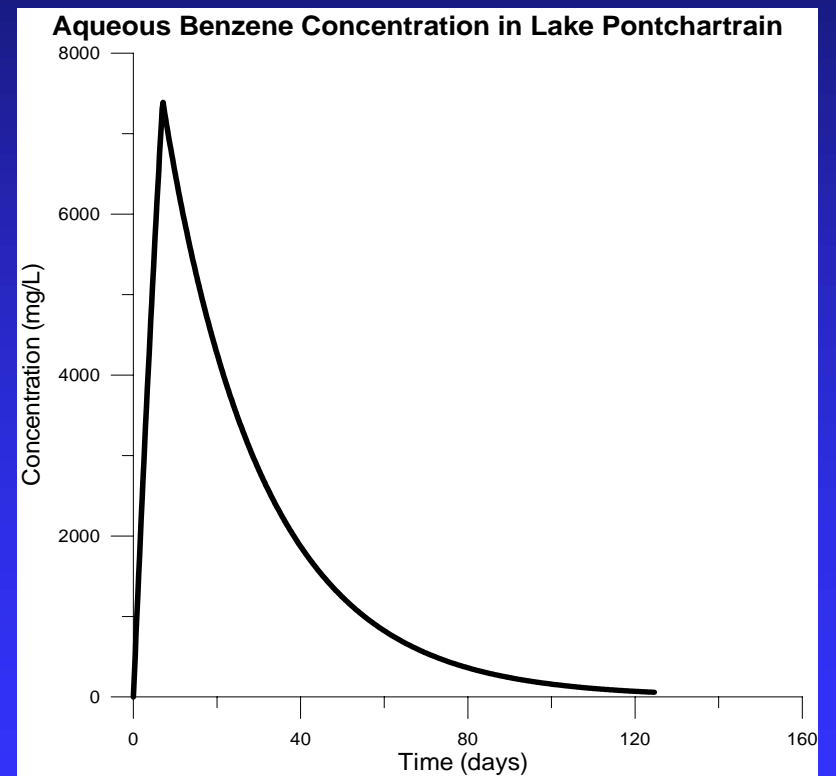
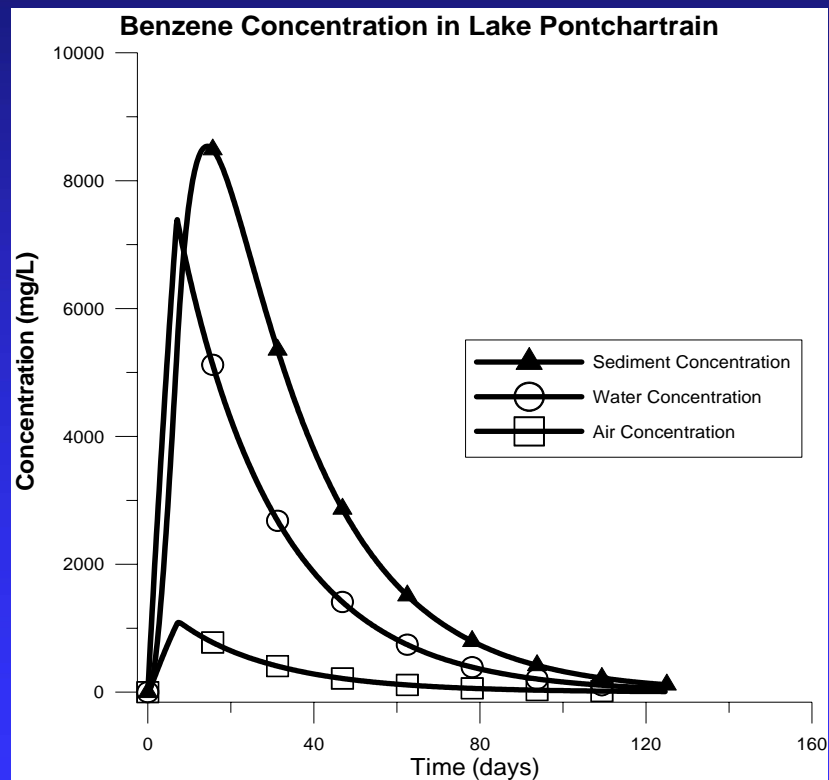


# Lindane Results

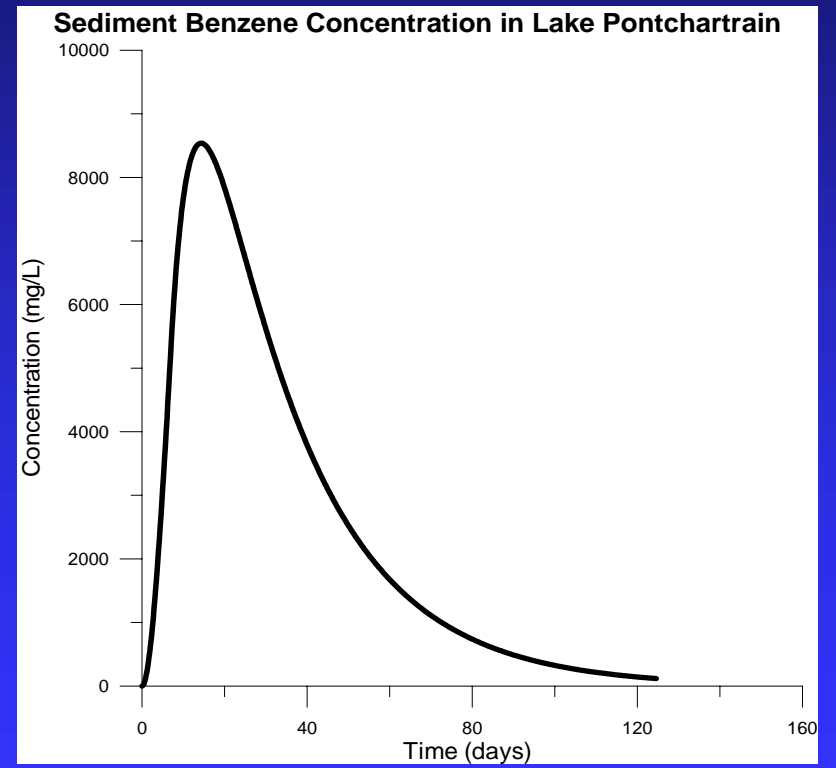
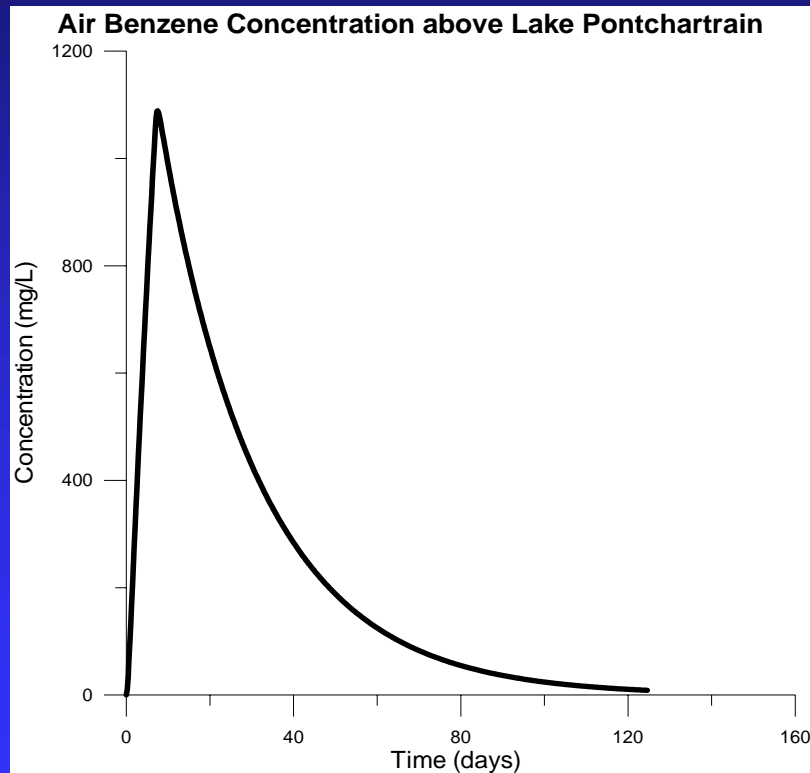




# Benzene Results



# Benzene Results



# Some Observations

- Air Phase recover quickest for all three contaminants
- As Benzene is more volatile, it partitions into air sooner and removed from the system – about 1 year
- PCB stays longest – 81 years
- All three chemicals stay longest in the sediments
- Benzene partitions more proportionally among three phases



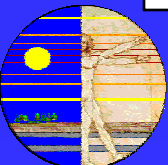
# Sensitivity Analysis - PCB

Parameter	Change	Time	Percent Change	Parameter	Change	Time	Percent Change
<b>Kaw</b>	10%	80.902	0.00405	<b>ka</b>	10%	81.307	0
	-10%	81.718	-0.00411		-10%	81.307	0
	20%	80.502	0.00805		20%	81.307	0
	-20%	82.135	-0.00828		-20%	81.307	0
<b>Ksw</b>	10%	81.359	-0.00052	<b>Qres</b>	10%	81.598	-0.00291
	-10%	81.256	0.00051		-10%	80.936	0.00371
	20%	81.41	-0.00103		20%	81.815	-0.00508
	-20%	81.21	0.00097		-20%	80.457	0.0085
<b>kw</b>	10%	81.307	0	<b>Qdep</b>	10%	80.982	0.00325
	-10%	81.313	-6E-05		-10%	81.621	-0.00314
	20%	80.301	0.01006		20%	80.64	0.00667
	-20%	81.315	-8E-05		-20%	81.895	-0.00588
<b>ks</b>	10%	74.321	0.06986	<b>Qair</b>	10%	81.307	0
	-10%	89.743	-0.08436		-10%	81.307	0
	20%	68.442	0.12865		20%	81.307	0
	-20%	100.137	-0.1883		-20%	81.307	0



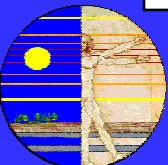
# Sensitivity Analysis - Lindane

Parameter	Change	Time	Percent Change	Parameter	Change	Time	Percent Change
<b>Kaw</b>	10%	13.234	0.00025	<b>ka</b>	10%	13.259	0
	-10%	13.285	-0.00026		-10%	13.259	0
	20%	13.207	0.00052		20%	13.259	0
	-20%	13.311	-0.00052		-20%	13.259	0
<b>Ksw</b>	10%	13.746	-0.00487	<b>Qres</b>	10%	13.302	-0.00043
	-10%	12.844	0.00415		-10%	13.318	-0.00059
	20%	14.309	-0.0105		20%	13.147	0.00112
	-20%	12.498	0.00761		-20%	13.38	-0.00121
<b>kw</b>	10%	13.067	0.00192	<b>Qdep</b>	10%	13.348	-0.00089
	-10%	13.438	-0.00179		-10%	13.164	0.00095
	20%	12.892	0.00367		20%	13.424	-0.00165
	-20%	13.633	-0.00374		-20%	13.076	0.00183
<b>ks</b>	10%	12.905	0.00354	<b>Qair</b>	10%	13.259	0
	-10%	13.698	-0.00439		-10%	13.259	0
	20%	12.667	0.00592		20%	13.259	0
	-20%	13.993	-0.00734		-20%	13.259	0



# Sensitivity Analysis - Benzene

Parameter	Change	Time	Percent Change	Parameter	Change	Time	Percent Change
<b>Kaw</b>	10%	1.012557	0.0001484	<b>ka</b>	10%	1.0245	2.897E-05
	-10%	1.04509	-0.00017693		-10%	1.03025	-2.853E-05
	20%	1.577626	-0.00550229		20%	1.02226	5.137E-05
	-20%	1.066781	-0.00039384		-20%	1.0331	-5.703E-05
<b>Ksw</b>	10%	1.0371	-9.703E-05	<b>Qres</b>	10%	1.027397	0
	-10%	1.018265	9.132E-05		-10%	1.027397	0
	20%	1.046233	-0.00018836		20%	1.027397	0
	-20%	1.009703	0.00017694		-20%	1.027397	0
<b>kw</b>	10%	0.985731	0.00041666	<b>Qdep</b>	10%	1.027397	0
	-10%	1.073059	-0.00045662		-10%	1.027397	0
	20%	0.946918	0.00080479		20%	1.027397	0
	-20%	1.123288	-0.00095891		-20%	1.027397	0
<b>ks</b>	10%	1.026826	5.71E-06	<b>Qair</b>	10%	0.998858	0.00028539
	-10%	1.027968	-5.71E-06		-10%	1.059361	-0.00031964
	20%	1.026256	1.141E-05		20%	0.973174	0.00054223
	-20%	1.028539	-1.142E-05		-20%	1.09589	-0.00068493



# Observations about Sensitivity Analysis (1)

- The most important parameter is sediment reaction rate constant ( $k_s$ ) – derived from half lives
- The higher the half life in sediment, longer it takes the lake to recover
- The second most effective parameter is sediment-water mass transfer rate ( $K_{sw}$ ). When the contaminant passes to sediment, it takes it longer to get out of the system.
- On the other hand, air-water mass transfer rate ( $K_{aw}$ ) has the inverse effect. As the contaminant passes into air, it is removed from the system quicker, due to faster decay and air outflow





# Observations about Sensitivity Analysis (2)

- Benzene is more sensitive for parameter changes.
- Benzene is more volatile, thus when air-water mass transfer coefficient is higher, removal of benzene from the system is quicker



# Conclusion

- Hydrophobicity. Higher the octanol-water partition coefficient, longer it will take a lake to replenish (PCB – 6.6; Benzene – 2.13; Lindane – 3.70)
- Volatile compounds will be removed faster, however will create air pollution problems in the immediate vicinity
- During the first couple of weeks following the dumping of the flood waters, some living organisms must have been harmed as the contaminants reach very high concentrations in the lake



# Ongoing Work:

- Inclusion of bioaccumulation module to this model.
- Consider speciation.
- Develop a dynamic model, which also has a spatial variability.
- Uncertainty analysis.



**For additional information or questions, you may contact:**

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*<http://www.ce.gatech.edu/research/MESL/>*

